

Amendments to the Specification:

Please substitute page 14, line 13 to Page 15, line 27 with the following amended paragraphs:

The construction of the airflow sensor 10 is similar to that mentioned with reference to Figs. 1 to 3. In a state where a plurality of airflow sensors 10 are formed on the semiconductor wafer 40, the disconnection portion 16 in Fig. 1 does not switch into the disconnecting condition yet, but remains in a conducting condition. In addition, the second lead conductors ~~15H1, 16H2~~ 15H2 and 15H3 in Fig. 1 are electrically connected in series through the second lead conductor 15H. With respect to the airflow sensors 10 arranged in a matrix form, an electrode 14H_{Lm}, 14H_{Ln}, ~~βββ~~ is formed at every member on the left side of the airflow sensors connected in series in each member, while an electrode 14HR common to the respective members is formed on the right side of the airflow sensors connected in series in each member.

In this case, the heat generating resistor 12H in Fig. 1 is used in a state heated to assume a temperature higher by approximately 100_C to 150_C than an ambient temperature on the basis of the resistance value of the temperature measuring resistor ~~12L~~ 12C. Since the ambient temperature increases to approximately 100_C due to the intake air of the motor vehicle, the heat generating resistor 12H is heated up to approximately 200_C to 250_C. For this reason, it was found that, if the airflow sensor is put to use for a long time, its deterioration grows gradually to cause variations in resistance. In response to the variation in resistance value, the flow rate characteristic of the thermal type airflow sensor 10 varies, with its lowered

reliability. Therefore, study was made about an aging treatment to prevent the variation in resistance value during the practical use by energizing and heating the heat generating resistor 12H in advance before use for promotion of its deterioration. The aging treatment is achievable, for example, by supplying a predetermined current to between the electrodes 14H1 and 14H2 shown in Fig. 1. However, it was found that the aging treatment at every airflow sensor creates a problem of a low working efficiency, for that the size of the airflow sensor 10 is as small as 2.5 mm _ 6 mm and each of the electrodes 14H1 and 14H2 is also shaped into a square whose one side is as small as 100 μm. As will be described later with reference to Figs. 8 to 13, as the energization condition, the energization time is required to be approximately 24 hours.

Please substitute page 16, line 25 to Page 17, line 11 with the following amended paragraphs:

On the other hand, in this embodiment, by measuring a resistance value between the electrodes 14HLm and 14HR shown in Fig. 6, it is possible to facilitate the inspection as to whether or not damaged sensors exist in a plurality of (for example, ~~40~~ forty) airflow sensors 10 connected between the electrodes 14HLm and 14HR. Likewise, the inspection for a plurality of sensors in the other members is possible. Since the probability of the occurrence of broken sensors is not very high, the collective inspection for the absence of broken sensors of the ~~40~~ forty sensors allows the inspection operation to be accomplished

for a short time. If the inspection has proven that the ~~40~~ forty sensors include some broken sensors, then it is possible to specify that broken sensor in a manner that the inspection of the sensors is made individually.

Please substitute page 17, line 20 to Page 18, line 9 with the following amended paragraphs:

Both end portions of the heat generating resistor 12HB are connected through first lead conductors 13H1B and 13H2B to electrodes 14H1B and 14H2B, respectively. A second lead conductor 15H1B connected to the electrode 14H1B is connected to an electrode 14H3A of the airflow sensor 10A. A second lead conductor ~~15H2~~ 15H2B connected to an electrode ~~14H2~~ 14H2B is connected through a narrow section 16B' and a second lead electrode ~~15H3~~ 15H3B to an electrode 14H3B. A heat generating resistor 12HA of the airflow sensor 10A is connected to an electrode 14H3A through a first lead conductor 13H2A, an electrode 14H2A, a second lead conductor 15H2A, a narrow portion 16A' and a second lead conductor 15H3A. In addition, a heat generating resistor 12HC of the airflow sensor 10C is connected to the heat generating resistor 12HB through a first lead conductor 13H1C, an electrode 14H1C and a second lead conductor 15H1C. In this way, the respective heat generating resistors 12HA, 12HB and 12HC are in series connection with each other.